

2-Years progress WORKSHOP

BOOSTING HIGH-PERFORMANCE MATERIALS FOR ENERGY INTENSIVE INDUSTRIES

Thursday 1st December 2022 9:30-12:00 CET



Development Of High Entropy Alloys-HEAs-For High Temperature Applications

Dr. Pilar Rey Rodriguez





Seamthesis

🕭 Constellium 🛛 ArcelorMittal



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The project has received funding from the European Union's Horizon 2020 research and innovation program under Grant Agreement N° 958374.

WP4 Targets

Our main Objective: to develop new HEAs by atomization to be printed using laser based-AM processes to be validated in Ells test cases

O4.1. To develop innovative HEA materials with improved high-temperature resistance properties (i.e., high-temperature strength and creep) and provide novel protective coatings based on HEA composites allowing high-temperature wear performance of coated components.

O4.2. To develop novel multi-component equiatomic HEA powders suitable for powder based AM process using gas atomization technique.

O4.3. To determine optimum process conditions for laser-based additive manufacturing of HEA materials **O4.4**. To correlate HEAs' composition and powder characteristics to their microstructure and properties attained by means of laser-based manufacturing processes, feeding and closing the loop with WP₂





¹ Fibre Optic Sensors ² Laser based Powder Bed Fusion ³ Laser Based Directed Energy Deposition ⁴ThermoCalc ⁵ Density Functional Theory ⁴ Mechanical Alloying

⁵ Laser Cladding

WP4 in ACHIEF Value Chain



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<u>Materials objective</u>: good quality with high temperature properties (tensile and creep resistance for AM and wear for LC)

SoA-HESA: Ni58,2Al10C013,8Cr6,3Fe4,9Ti6,8 <u>High Entropy Super alloy</u>

OBJECTIVE

To promote high rate of hardening γ ' phase in a γ

matrix, looking for higher volume fraction and

diametre of γ'

AI-MEA: Ni28,6Fe28,6Co28,6Al14,3 Medium Entropy complex concentrated alloy

OBJECTIVE:

Promoting multi-scale microstructure of fine scale FCC+LI2 grains mixed with B2+BCCgrains



Wei-Chih Lin, et al., Additive Manufacturing, 36, 2020, 101601







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HEAs atomization

WP4: Materials

To atomize the lab powder batches the steps below were followed

- I. Preparing of the pre-alloy
- Melting/Solidifying the alloy several times to homogenize
- Induction heating for melting the pre-alloy and crucible solidification
- Solidified ingot sectioning to be leaded in the atomization crucible
- II. Atomization of batches of 15 kg at VTT with Hermiga 75/5VI gas atomizer
- The pre-alloy batches were heated to melting temperature and over heated to ensure free flow of the melt stream
- The melt was fed through aluminium oxide nozzle and the melt stream was atomized with high-pressure in argon gas. The powder was then left to cool inside the atomization chamber in argon to avoid oxidation
- Two fractions were produced:
- a) Chamber fraction: the main fraction, was sieved into suitable Particle Size Distribution (PSD), for LPBF (<45µm) & DED-LB (+45 125µm)
- b) Cyclone fraction is very fine, so unusable for AM







Source: VTT atomizer

<u>Chemical and crystalline powder analysis</u>: Energy-dispersive X-ray spectroscopy (EDS) & X-Ray Diffraction (XRD)

- -Got <1at-% accuracy for the final composition
- Ti segregation in inter-dendritic regions in SoA-HESA
 No element segregation observed in AI-MEA

SoA-HESA













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Thermal behaviour powder analysis: Differential Thermal Analysis (DTA)

- In air, 1 exo peak at 800°C (phase transformation) and 980°C (exo) that is associated with a great loss of weight (oxidation & evaporation)
- In Ar, defined peaks disappear, but still weight loss is observed with violent oscillations
- In air, three peaks (exo) with weight gain probably due to oxidation
- In Ar, defined peaks disappear, and weight changes are almost neglectable

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Powder morpholyg and Particle Size Distribution: Scanning Electron Microscopy (SEM) & Laser Diffraction

AI-MEA

- Typical gas atomized powder spherical morphology is shown
- Satellite formation avoided

PSD homogeneous

SoA-HESA





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ED-I

HEAs mixing: HEAs based MMCs

- Mixes prepared in Turbula mixer
- BPR with YSZ balls 1:1 used
- \Box 24h mixing
- Different ratios and type of reinforcement

Sample	Hall Flow	N ^o measurements	Tap(yes/no)
		Torreproducibility	
HESA1	17,9	6	
HESA1HESA1+	19,2	5	
4%vol. n-TiC			
HESA1HESA1+	20,7	13	Yes (occasionally)
8,5%vol. n-TiC			
HESA1HESA1+	24,0	14	Yes (all measurements)
15%vol. n-TiC			

- ✓ After mixing, particles remained almost spherical
- ✓ EDS analysis confirmed that the n-TiC remains in the outer part of HESA1 particles forming like a shell

sto +1	nass percent (%)									
a start the	Spectrum	с	0	Al	Si	Ti	Cr	Fe	Co	Ni
	1 2 3 4	23.26 1.70 4.12 7.35	9.93 0.13 0.36 1.00	3.26 2.75 2.76 5.40	0.09 11.58 1.41 0.11	61.74 3.91 3.04 3.78	0.00 5.89 5.99 5.76	0.00 2.93 2.80 2.57	0.33 14.39 16.78 14.68	1.38 56.72 62.73 59.35
	Mass percent	t (%)								
31.1	Spectrum	с	0	Al	Si	Ti	Cr	Fe	Co	Ni
	1	26.23	9.74	1.17	0.00	61.81	0.00	0.00	0.00	1.05

EDS analysis on the cross section of a SEM micrograph on a 4%voln-TiC/HESA1 (top) & 15%vol n-TiC/HESA1 particles (bottom)

11.59 0.78 4.42 0.23 3.04 6.18 2.58 14.88 56.30 5.04 0.61 4.44 0.02 3.81 5.84 3.01 15.45 61.79



SEM micrographs of pre-alloyed batches of HESA1 with 4, 8.5 and 15%vol. n-TiC from the left to the right showing size and shape of the particles.







Laser Based Powder Bed Fusion (LPBF)- SoA HESA

MAIN RESULTS:

- LPBF conditions allow to obtain parts with **99.2-100%** relative density
- A network of cracks detected by μCT and OM; surface crack density evaluated: 3.6 mm/mm²
- Cracks at the High Angle Grain Boundaries, following the solidification cells joints.

- Presence of γ et γ' confirmed by XRD; Fraction of 42% of γ' phase consistent with predictions; γ' nano-precipitates of size < 5 nm detected by TEM
- After solution annealing + precipitation hardening, γ' precipitates, spherically shaped and enriched in Al, Ti and Ni have significantly increased and represent 50% of the surface

LPBF samples on their baseplate





SEM-BSE image and ESBD maps in plane XZ



 ϑ -2 ϑ XRD on top surface of a LPBF cube



Duplex γ/γ 'microstructure after heat treatment (SEM)





Laser Based Directed Energy Deposition (DED-LB)- SoA HESA





- Tracks and overlaps do not give any apparent problems
- Some material is ejected during manufacturing promoting severe fissures as grow in Z direction
- Analysis of ejected particles show large quantities of O and C (as DTA predicted)
- Improving argon protection, the quality is greatly enhanced although there were still cracks
- Manufacturability is an important criteria not considered in AI. Oxidation problem nor detected by CALPHAD

SoA-HESA has been used for cladding AI HESA will be scale up for 3D printing





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Laser Based Powder Bed Fusion (LPBF)- AI-MEA

MAIN RESULTS:

- LPBF conditions allow to obtain parts with 99.74-100
 % relative density
- No cracks have been detected in AI-MEA

As built LPBF samples





Direct aging of LPBF samples



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Only aging for tensile, SEM, XRD and tomography

• 2 different TTs have been selected and applied.

One will be used in SEM (H+A)



Laser Based Directed Energy Deposition (DED-LB)- AI-MEA

DED-LB





- Good manufacturability without remarkable defects. Less power needed than in SoA-HESA
- Good compromise between strength & ductility (as built condition)

Rp0,2 (Mpa)	Rm (Mpa)	A (%)	Z (%)
735	918	17	27

- Solidification microstructure with recrystallized zones
- > No detectable micro-segregation of elements

IN PROGRESS

- Microstructural analysis in as-built condition, including fracture.
- FEM simulation
- Thermal treatment definition & application
- Tensile at@800°C (as built VS TTed)
- Planned creep tests (1yr-ahead)

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Laser Based Directed Energy Deposition (DED-LB)- AI-MEA

WP4: Processes

Heat Treatment



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Laser Cladding- SoA-HESA

- Reinforcement: n-TiC (4, 8.5 & 15% vol.) and m-TiC (60% vol.)
- Laser power: 500-1100
- Speed: 5-30mm/s
- Powder Flow: 2-8g/min for nano / up to 25g/min with micro
- Gas Flow: 27L/min
- Clads: 1 & 2 layers
- Overlap: 55% and 75%



- Nano-reinforcement promotes higher dilution
- Better hardness achieved is around 450Hv







- Micro-reinforcement promotes lower dilution
- Better hardness achieved is > 850Hv
- Large dispersion due to the size of the reinforcement





OUTLOOK/NEXT STEPS IN WP4

DED & PBF

- Deeper microstructural analysis in as-built condition, and comparison after thermal treatment.
- Thermal treatment application to testing specimens
- Tensile at@800°C (as built VS TTed)
- TT- creep tests
- To scale up atomized AI-MEA up to 150kg (for WP7)

LC

- Process parameters optimization
- HT wear tests for HEAs MMCs coatings







Thank you

AIMEN: Pilar Rey Rodriguez: prey@aimen.es VTT:Tom Andersson: Tom.Andersson@vtt.fi VTT: Tomi Suhonen: Tomi.Suhonen@vtt.fi CEA: Thierry Baffie: thierry.baffie@cea.fr SEAMTHESIS: Maria Rita Ridolfi: mariarita.ridolfi@seamthesis.com CONSTELLIUM: Ariane Viat: ariane.viat@constellium.com ARCELORMITTAL: Fermin Agreda: fermin.agreda@arcelormittal.com

